## Appendix H <br> Driveability Index Analysis

Table 1 shows the data on $\mathrm{DI}^{*}$ and other gasoline properties from the sampling data reported by the Association of American Automobile Manufacturers for "Los Angeles" and "San Francisco" in the summer of 1998.

These data have been fit with two linear models:

$$
\begin{aligned}
& \text { DI }(1)=a+b^{*} R V P+b^{\prime} *[1, \text { if grade }=r e g]+c^{*} \mathrm{~T} 50+d^{*} \mathrm{~T} 90 \text { and } \\
& \text { DI }(2)=a+b^{*} R V P+c^{*} \text { T50 }+d^{*} \text { T90 }
\end{aligned}
$$

The output of the regressions are:

|  | Coefficient | $\mathbf{p}$ (Significance) |
| :---: | :---: | :---: |
| DI (1), $\mathbf{R}^{\mathbf{2}}=\mathbf{. 9 9 1}$ |  |  |
| Intercept | 242.3 | $<0.001$ |
| Regular | -3.171 | 0.09 |
| RVP | -8.331 | 0.10 |
| T50 | 3.234 | $<0.001$ |
| T90 | 0.9270 | $<0.001$ |
|  |  |  |
| DI (2), $\mathbf{R}^{\mathbf{2}}=\mathbf{0 . 9 9 2}$ |  |  |
| Intercept | 208.2 | $<.001$ |
| RVP | -5.510 | .28 |
| T50 | 3.395 | $<.001$ |
| T90 | .8559 | $<.001$ |

Although the significance values (p) for RVP are larger than is often accepted for including terms in multiple regression equations, the RVP terms have been kept as necessary surrogates for T10. The equation for DI (1) is preferable (when grade data are available) because of the lower p-value on RVP and because the coefficients for T50 and T90 are closer to their actual values, 3.0 and 1.0.

Since the coefficients for RVP are negative and actual RVPs are less than the inputs to the regressions (values in the table), using actual RVP as inputs to the equations leads to over-predicted values of DI. If the bias in the tabular RVPs is $0.36 \mathrm{psi}, \mathrm{DI}$ is over-predicted by $3{ }^{\circ} \mathrm{F}$ by DI (1).

[^0]Table 1
Inputs for DI Regression

| RVP' | Grade | RVP | T50 | T90 | DI |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 7.1 | Premium | 6.84 | 209 | 306 | 1143 |
| 7.1 | Premium | 6.84 | 201 | 292 | 1107 |
| 7.0 | Premium | 6.74 | 215 | 300 | 1157 |
| 7.2 | Premium | 6.94 | 209 | 305 | 1142 |
| 7.0 | Premium | 6.74 | 208 | 302 | 1136 |
| 7.0 | Intermed. | 6.74 | 209 | 305 | 1142 |
| 7.1 | Intermed. | 6.84 | 198 | 312 | 1107 |
| 6.7 | Regular | 6.44 | 192 | 291 | 1076 |
| 7.0 | Regular | 6.74 | 197 | 306 | 1101 |
| 7.0 | Regular | 6.74 | 188 | 308 | 1078 |
| 7.1 | Regular | 6.84 | 189 | 290 | 1064 |
| 7.1 | Regular | 6.84 | 199 | 318 | 1119 |
| 7.0 | Regular | 6.74 | 197 | 297 | 1100 |
| 7.1 | Regular | 6.84 | 201 | 318 | 1128 |
| 7.0 | Regular | 6.74 | 199 | 311 | 1112 |
| 7.1 | Regular | 6.84 | 194 | 314 | 1094 |
| 7.1 | Premium | 6.84 | 214 | 312 | 1169 |
| 7.0 | Premium | 6.74 | 211 | 300 | 1145 |
| 7.2 | Premium | 6.94 | 207 | 310 | 1140 |
| 6.8 | Premium | 6.54 | 212 | 314 | 1169 |
| 7.1 | Premium | 6.84 | 208 | 314 | 1150 |
| 7.3 | Premium | 7.04 | 207 | 320 | 1153 |
| 7.1 | Intermed | 6.84 | 201 | 309 | 1119 |
| 7.2 | Regular | 6.94 | 200 | 322 | 1128 |
| 7.2 | Regular | 6.94 | 187 | 298 | 1065 |
| 7.2 | Regular | 6.94 | 202 | 315 | 1130 |
| 7.0 | Regular | 6.74 | 212 | 319 | 1165 |
| 7.1 | Regular | 6.84 | 199 | 319 | 1122 |
| 6.9 | Regular | 6.64 | 199 | 312 | 1118 |
| 7.1 | Regular | 6.84 | 196 | 315 | 1106 |
| 7.0 | Regular | 6.74 | 199 | 311 | 1117 |


[^0]:    * Driveability Index is computed from points on the ASTM D 86 distillation curve for a gasoline: $\quad \mathrm{DI}\left({ }^{\circ} \mathrm{F}\right)=1.5 * \mathrm{~T} 10+3.0^{*} \mathrm{~T} \% 0+\mathrm{T} 90$

